

USAAEFA PROJECT NO. 89-06



PRELIMINARY AIRWORTHINESS EVALUATION OF THE UH-1H WITH HOT METAL PLUS PLUME INFRARED SUPPRESSOR AND INFRARED JAMMER

FINAL REPORT

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JUNE 1981



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The Preliminary Airworthmess Evalua	tion PAL) of the UH-IH.	with the Garrett AiResearch Infarared		
(IR) Suppressor and AN/ALO-144 IR Jammer installed, was conduct d at 1-dwards Air Force Base California, (elevation 2300 feet) and Bakersfield, California, (elevation 490 feet) using a IUH-411				
helicopter (S/N 69-15532); A total of 20.7 hours were flown during this test program. This PAF was				
an evaluation of a redesigned IR suppressor and IR januage installation for the UH-IH helicopter. The				
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both the standard and IR suppressor configurations. Phase II (29-April through-18 May-4981; 11, flight hours) was primarily a pressure and temperature survey of the IR suppressor configuration. The handling qualities of the UH-1H helicopter were essentially unchanged by the IR suppressor and II jammer installation tested. The previously reported degradation in directional stability was not observe during this test. The tail boom surface temperatures were generally higher than those reported by BH for the initial design and the structural implications of these higher temperatures should be investigated. One deficiency, the metal to metal contact between the engine exhaust ejector and the IR suppresso inner core support struts, was identified. Three shortcomings were also identified.	R I
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DEPARTMENT OF THE ARMY 143, US ARMY AVIATION RESEARCH AND DEVELOPMENT COMMAND 4300 GOODFELLOW BOULEVARD, ST. LOUIS, MO 43120

DRDAV-D

SUBJECT: USAAEFA Report, Preliminary Airworthiness Evaluation of the UH-1H

with Hot Metal Plus Plume Infrared Suppressor and Infrared Jammer,

USAAEFA Project No. 80-06

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- 1. The purpose of this letter is to establish the Directorate for Development and Qualification position on subject report. The report documents the test results of the subject evaluation and substantiates that the handling qualities of the JUH-1H with the Not Metal Plus Flume Suppressor are essentially the same as those of the standard UH-1H helicopter. The tail boom surface temperatures were generally higher than those reported by Bell Helicopter Textron for the initial design.
- 2. This Directorate agrees with the report's conclusions and recommendations. Additional design development is in progress by BHT under Army contract and further flight testing will be conducted which should accommodate the recommendations and conclusions of this report.

FOR THE COMMANDER:

CHARLES C. CRAWFORD, JR. Director of Development and Qualification

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TABLE OF CONTENTS

	Pag
TRODUCTION	
Do strangum I	
Background	
Test Objectives	
Description	
Test Scope	
Test methodology	
SULTS AND DISCUSSION	
General	
Handling Qualities	
General	
Control Positions in Trimmed Forward Flight,	
Static Longitudinal Stability	
Static Lateral-Directional Stability	
Maneuvering Stability	
Domain's Ctability	
Dynamic Stability	
Lew-Speed Flight Characteristics	
General	
Forward and Rearward Flight	
Sideward Elight	
Mission Maneuvering Characteristics	
Simulated Engine Failures	
Pressure Survey	
Temperature Survey	
Rehability and Maintainability	
General	
Phase I. Testing	
Phase II. Testing	
NCLUSIONS	
General	
Deficiency	
Shortcomings	
Specification Compliance	

TABLE OF CONTENTS

	Page
NTRODUCTION	
Background	
Test Objectives	
Description	•
Test Scope.	
Test Methodology	
itsi memology	•
ESULTS AND DISCUSSION	
General	
Handling Qualities	
General	
Control Positions in Trimmed Forward Flight	
Static Longitudinal Stability	
Static Lateral-Directional Stability	
Maneuvering Stability	
Dynamic Stability	
Low-Speed Flight Characteristics	
General	
Forward and Rearward Flight	
Sideward Flight	
Mission Maneuvering Characteristics	
Simulated Ungine Failures	
Pressure Survey	
Temperature Survey	
Reliability and Maintainability	
General	
Phase I. Testing	
Phase II. Testing	•
ONCLUSIONS	
General	
Deficiency	
Shortcomings	
Specification Compliance	
Specification Computation Control of the Control of	•
•	
FCOMMENDATIONS	

APPENDIXES

Α.	References	1.
		1.
C .	Instrumentation	2.
D.	Test Techniques and Data Analysis Methods	3
Ε.	Test Data	3
F.	Equipment Performance Reports	7

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INTRODUCTION

BACKGROUND

1. The United States Army requires a reduced infrared (IR) signature and increased protection from IR seeking weapons for its aircraft. To achieve these goals, the US Army contracted with Bell Helicopter Textron (BHT) to develop an installation to accommodate a Garrett AiResearch Manufacturing Company (Garrett) hot metal plus plume (HMPP) IR suppressor and an AN/ALQ-144 IR jammer on the UH-1H helicopter. BHT was required to prove feasibility of the HMPP IR suppressor design, conduct limited flight testing, and assess IR cooling. Flight testing of the initial design by BHT showed that the suppressor pressures and the suppressor and tail boom temperatures were acceptable; however, the directional stability characteristics of the aircraft were degraded. BHT initiated a redesign of the suppressor and jammer installation to reduce the airflow disturbance, which was believed to be causing the degradation of directional stability. The US Army Aviation Research and Development Command (AVRADCOM) directed the US Army Aviation Engineering Flight Activity (USAAFFA) to perform a preliminary airworthiness evaluation (PAF) of the UH-1H with the redesigned IR suppressor and jammer installation (ref. 1, app. A). A test plan (ref. 2) was submitted in January 1981 and an Airworthiness Release (ref. 3) was issued in February 1981.

TEST OBJECTIVES

- 2. The overall objectives of this PAI were to determine if the redesigned suppressor and jammer installation changed the handling qualities of the UI-IH and to conduct a survey of suppressor pressures and suppressor and tail boom temperatures.
- The specific test objectives were:
- a. To provide quantitative and qualitative flight test data of the aircraft handling qualities.
- b. To determine suppressor pressures and suppressor and tailboom temperatures.

DESCRIPTION

4. The UH-IH is a thirteen-place single engine helicopter using a single two-blade teetering main rotor and pusher tail rotor. The maximum gross weight of the helicopter is 9500 pounds. Power is provided by a Lycoming F53-L-13 free turbine engine rated at 1400 shaft horsepower (SHP). However, the helicopter is limited by the transmission to 1100 SHP. A more complete description may be found in the detail specification (ref. 5, app. A) and the operator's manual (ref. 4). The test helicopter was a JUH-IH, S.N. 69-15532. The significant external differences from the standard UH-IH were removal of the cargo hook and the addition of an airspeed boom, 9.5 feet long, mounted on the centerline of the helicopter at the base of the windshield center post. Internal differences consisted primarily of the instrumentation system. These differences had no significant effect on the flight test results.

5. The IR suppressor and jammer installation consisted of a Garrett HMPP IR suppressor, originally developed for the AH-IS helicopter, an AN/ALQ-144 IR jammer, and a redesigned aft engine cowl to support the suppressor and jammer. A more detailed description of the IR suppressor and jammer installation is provided in appendix B.

TEST SCOPE

6. Flight testing was conducted at Edwards Air Force Base, California, (elevation 2302 feet) and Bakersfield, California, (elevation 490 feet) during the period 16 January 1981 through 18 May 1981. A total of 16 flights were conducted during which 20.7 hours were flown. Tests were conducted in two phases. The first phase consisted of an evaluation of handling characteristics with primary emphasis on the lateral-directional stability characteristics of the air raft with the 1R suppressor and jammer installed. Data were also taken with the aircraft in the standard configuration as a basis for comparison. The second phase tests were primarily a survey of IR suppressor pressures and suppressor and tailboom temperatures. Flight restrictions and operating limitations contained in the airworthiness release (ref. 3, app. A), and the operator's manual (ref. 4) were observed. Where possible, flight test data were compared with the applicable specifications (refs. 1 and 6) and with data obtained from previous tests of the UH-1H (refs. 7, 8, and 9). Flight tests were conducted under the conditions specified in table 1.

TEST METHODOLOGY

7. Established flight test techniques were used throughout this evaluation (ref 10, app A). Test methods used are briefly discussed in the Results and Discussion section of this report. The handling qualities rating scale (HQRS) shown in figure 1, appendix D, was used to supplement pilot comments on handling qualities. All flight test data, during the handling qualities tests, were obtained from calibrated test instrumentation and were recorded on magnetic tape. Data obtained during the pressure/temperature survey were recorded both on magnetic tape (pressures) and by hand from cockpit instrumentation (temperatures). A detailed listing of the test instrumentation is contained in appendix C. The definitions of deficiencies and shortcomings used during this test and data analysis methods used are presented in appendix D.

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Table 1 Test Combines

	,	Table 1 Test	Conditions		, ··
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RESULTS AND DISCUSSION

GENERAL

This PAE was an evaluation of a redesigned IR suppressor and IR jammer installation for the UII-III helicopter. The initial design was reported by BHT (ref 9, app A) to have caused a degradation in directional stability. The installation was redesigned to reduce the airflow disturbance over the vertical stabilizer. This evaluation was conducted in two phases. Phase I was a comparative evaluation of handling qualities of the UH-III in both the standard and IR suppressor configurations. Phase II was primarily a pressure and temperature survey of the IR suppressor configuration. The handling qualities of the UH-III helicopter were essentially unchanged by the IR suppressor and IR jammer installation tested. The previously reported degradation in directional stability was not observed during this test. The tail boom surface temperatures were generally higher than those reported by BHT for the mitial design and the structural implications of these higher temperatures should be investigated. One deficiency, the metal to metal contact between the engine exhaust ejector and the IR suppressor innercore support struts, was identified. No new specification non-compliances were identified as a result of the IR suppressor installation on the UH-III helicopter. Three shortcomings were identified.

HANDLING QUALITIES

General

9. The handling qualities of the UH-1H were evaluated at the test conditions listed in table 1. All tests were conducted using standard flight test techniques (ref 10, app A). Tests were conducted with the IR suppressor and IR jammer installed and repeated with the standard UH-1H tailpipe installed. Data obtained from tiese tests were compared to determine if the handling characteristics of the UH-1H were significantly affected by the installation of the IR suppressor system. Additionally, data were compared with previous tests of a standard UH-1H (refs 7 and 8) and a previous design of the IR suppressor installation (ref 9). Test results show that the handling qualities of the UH-1H are essentially unchanged by the installation of the HMPP IR suppressor and AN ALQ-144 jammer.

Control Positions in Trimmed Forward Flight

10. The control positions were evaluated in level flight and in climis and descents. Test results are presented in figures 1 through 6, appendix F. The control positions in trimmed forward flight were essentially unchanged from the standard UH-1H.

Static Longitudinal Stability

11. Tests were conducted in 'evel flight for both the standard and the IR suppressor configurations. Climbs were conducted at intermediate rater power (IRP) and descents were conducted at approximately 10 pounds per square inch (psi) indicated engine torque, in the IR suppressor configuration only. Data are presented in figures 7 through 10, appendix F. The aircraft exhibited positive longitudinal control force and position stability for all conditions tested. Qualitatively, the stability characteristics observed during climbs and descents were similar to those of the standard. UH-111 aircraft. The static longitudinal stability was essentially unchanged by the installation of the IR suppressor assembly.

Static Lateral-Directional Stability

12. The tests were conducted in level flight, climb, and descent. The standard configuration was evaluated in level flight only. Test results are presented in figures 11. through 14, appendix 15. The test arcraft exhibited both positive directional stability and positive dihedral effect. A direct comparison between the IR suppressor configuration (fig. 11) and the standard configuration (fig. 12) shows essentially no change in lateral-directional stability characteristics. Stability characteristics during climbs and descents qualitatively were unchanged from standard UII-111 arcraft. The static lateral-directional stability of the UII-111 aircraft was essentially unchanged by the installation of the IR suppressor system.

Maneuvering Stability

13. The mane overme stability characteristics were evaluated using constant airspeed left and right turns with the collective control fixed at the initial trim position. Flight test data for both the IR suppressor installation and the standard UH-1H are presented in figures (5 and 16, appendix 1, respectively. The stick-fixed stability (control position vs load factor) was positive for the load factors tested. Control position gradients were similiar for both configurations, Qualitatively there was no change in the stack tree stability (control force vs load factor). The maneuvering stability characteristics were essentially the same as those noted for the standard UH-1H.

Dynamic Stability

- 14. The longitudinal dynamic stability characteristics were evaluated in level flight. Data are presented in figures 17 through 19, appendix 1. Both the short-term and long-term dynamic response was essentially deadbeat and no difference was noted between the IR suppressor and standard tailpipe configurations.
- 15. The lateral-directional dynamic stability characteristics were evaluated in level flight for both the standard and the IR suppressor configurations. Directional control doublets and pulses were the most effective methods of exciting the lateral-direction oscillation. Data for both configurations are presented in figures 20 through 28, appendix I. A heighty damped foll-yaw oscillation was observed for both configurations tested. The installation of the IR suppressor system had no significant effect on the lateral-directional characteristics of the standard UH-IH helicopter.

Low-Speed 1-light Characteristics

General

16. Testing was accomplished using the ground piece vehicle method at a constant skid height of 10 feet in winds of 5 knots or less. Data were recorded at 5 knot increments from a lover to 40 knots forward, 30 knots rearward, and 35 knots sideward flight. Control excursions, as presented on the data plots, give an indication of pilot work load and were supplemented by pilot qualitative comments. The results of these fests were compared to those previously reported for the standard UT-HI helicoptar (refs.? and 8, app. Vr. 16. low speed handling qualities of the UH-HI equipped with the IR suppressor and imminer were essentially unchanged from the standard configuration.

Forward and Rearward Flight:

17. The results of the forward and rearward flight tests are presented as figures 29 and 30, appendix E. Figure 30 shows that at rearward airspeeds of 16 to 29 knots true airspeed (KTAS) (forward og 132.1) less than 16 percent aft longitudinal control margin remained. The aft longitudinal control inputs which were necessary to control the aircraft pitching motion within the 10 to 15 knot range resulted in a higher pilot work load (HQRS 5), as documented in reference 8, appendix A. Depending on pilot seat position, the pilot may contact equipment attached to his survival vest with the cyclic prior to reaching the full aft longitudinal control position. The lack of adequate longitudinal control margin within the specified limit of the operator's manual was previously reported as a deficiency (ref 7) and was not a result of the IR suppressor and jammer installation.

Sideward Flight:

18. The results of the left and right sideward flight tests are presented as figures 31 and 32, appendix t. The longitudinal trim shift of approximately 2.5 inches during left sideward flight between 8 and 15. KTAS is characteristic of the standard UH-1H (ref. 8, app. A) and contributed to high pilot work load (HQRS 5). Figure 32, shows that at the left sideward flight limit of 35 KTAS the right directional control pedal stop was contacted. Inadequate directional control margin was previously reported as a deficiency for the standard UH-1H (ref. 7) and was not a result of the IR suppressor and immer installation.

Mission Maneuvering Characteristics

19. Confined area operations, pinnacle operations, nap of the earth and contour flight, non-precision and precision instrument approaches were performed in light to moderate turbulence to evaluate aircraft handling characteristics in turbulence. No degredation of handing qualities due to the IR suppressor installation was observed during operation in turbulence. The aircraft response from light to moderate turbulence was essentially unchanged from the standard UH-1H.

Simulated Engine Failures

20. Simulated engine failures were performed in level flight by rapidly rolling the throttle to the flight idle detent. Flight controls were near fixed until activation of the low main rotor speed audio tone. Data are presented in figures 33 through 36, appendix F. Tests showed no degredation of handling qualities due to the IR suppressor installation. The aircraft response to simulated engine failures was essentially unchanged from the standard UH-IH.

Pressure Survey

21. Static and total pressures surrounding the IR suppressor were recorded at the test conditions listed in table 1. The type and location of the pressure sensors are shown in table 1, appendix C. Pressure data is provided in tables 1 and 2, appendix E.

Temperature Survey

22. Temperatures surrounding the IR suppressor and along the tail boom were recorded at the test conditions listed in table 1. The locations of temperature sensitive tapes and thermocouples are shown in table 2, appendix C. All recorded thermocouple and temperature sensitive tape data are presented in tables 3 and 4, appendix E. Generally higher temperatures were observed than those previously reported by BHT (ref 9, app A) for the initial IR suppressor installation. This may be accounted for by the redesign of the IR suppressor installation which resulted in a 5 degree depression of the IR suppressor exhaust centerline. A comparison of maximum tail boom temperatures obtained during this test with those previously reported by BHT is shown in figure 1. An increase of 80° F during hover and 140° F during low speed flight was observed. Further investigation to determine the structural implications of the high tail boom temperatures observed during this test should be conducted prior to release for field operations.

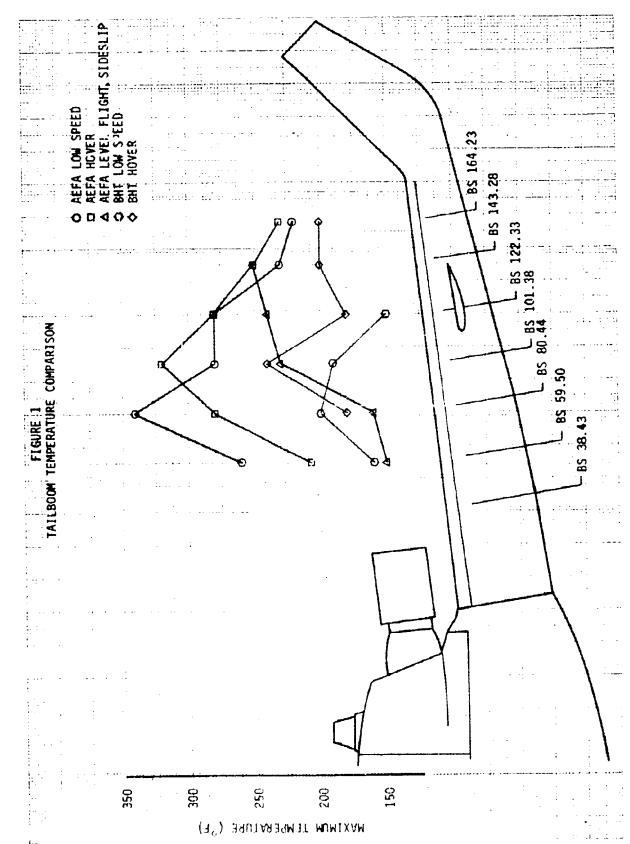
RELIABILITY AND MAINTAINABILITY

General

23. The reliability and maintainability of the IR suppressor and related components of the installation were evaluated during both phases of testing. Phase I testing was performed using an IR suppressor (AiResearch S N 39-D1) which had a total of 235 flight hours when it arrived at USAALFA. A new IR suppressor (AiResearch S/N 129-147) was provided for phase II testing. The new IR suppressor incorporated modifications which were designed to prevent cracking around the inner core support struts.

Phase I Testing

- 24. The IR suppressor was-found to be susceptible to cracking around the struts which support the inner core of the suppressor unit. When the unit arrived at USAAFFA, numerous cracks were discovered. It appeared that if flights were conducted without first having the unit repaired, small triangular pieces of metal could be dislodged from the inner core of the unit. The unit was repaired by welding prior to installation. Upon completion of Phase I tests, (9.5 flight hours) cracks were again observed in the area where the repair had been made as well as small cracks at each of the remaining struts. The susceptibility of the IR suppressor unit to cracking is a shortcoming which should be corrected prior to follow-on redesign.
- 25. When attempting to latch the engine cowling open using the latch provided near the tail boom attachment point, the engine cowling contacted the IR suppressor fairing and could not be latched without deforming the engine cowling. If not latched, the engine cowling could cause damage to the fins on the tailpipe of the suppressor. The IR suppressor installation should allow the engine cowling to be latched open in the same manner as the production UH-III. The inability to latch the engine cowling in the open position is a shortcoming, which should be corrected prior to follow-on redesign.
- 26. A small maintenance-inspection door was provided on the left side of the IR suppressor fairing only. To facilitate maintenance and preflight inspections, a door

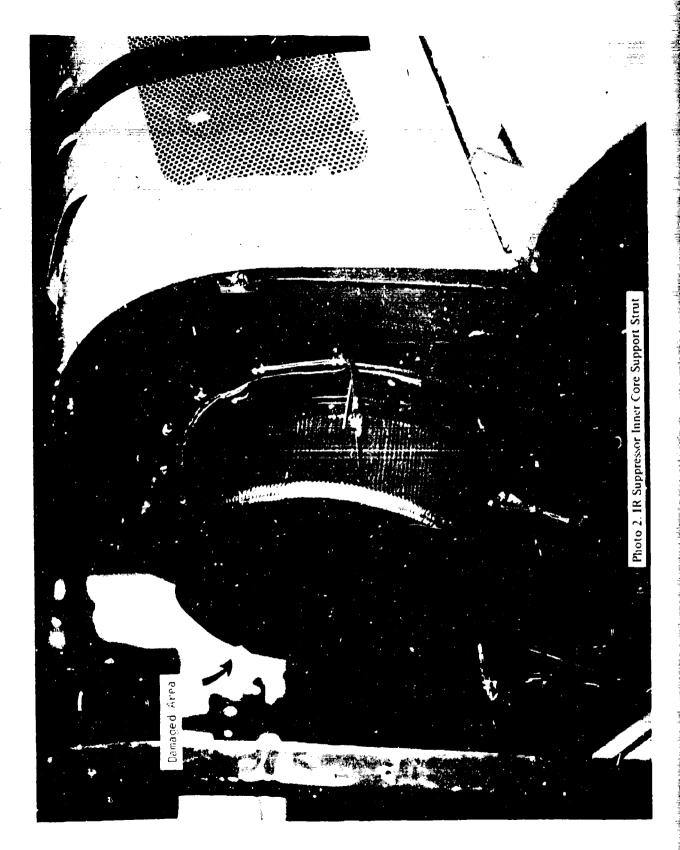


should be provided on the right side as well. The lack of a maintenance-inspection door on the right side of the suppressor fairing is a shortcoming, which should be corrected prior to follow-on redesign.

Phase II Testing

- 27. During removal of the new IR suppressor, warpage of the aft outer ring portion of the exhaust ejector (Bell part no. 205-068-217-101) and metal-to-metal contact between the exhaust ejector and suppressor were discovered. Score marks on the leading edge of the IR suppressor struts plus warpage and torn metal at the aft edge at the 1 o'clock position on the exhaust ejector indicates ejector movement of $\pm 1/2$ inch against the struts (photos 1 and 2). The IR suppressor struts and exhuast ejector areas were carefully inspected on each daily aircraft inspection. Damage to the above was discovered after 3.1 hours of low speed flight testing and 1.5 hours of ferry flight time to the test site at Bakersfield, California and back. Continued metal-to-metal contact between the engine exhaust ejector and the IR suppressor support struts will cause structural damage to both components and a significant reduction in service life. Should such structural damage go undetected, portions of either component could break loose and cause damage to the airframe. An Equipment Performance Report (EPR) (80-06-1) shown in appendix F was submitted during this test. The metal-to-metal contact between the engine exhaust ejector and the IR suppressor innercore support struts due to the positioning of the IR suppressor is a deficiency which should be corrected prior to further operation with the IR suppressor installed.
- 28. The IR suppressor (S/N 129-147) exhibited four burned areas on its outer surface immediately aft of the fiberglass fairing (near the trailing edge of the IR suppressor struts). The largest burned area was approximately 6 by 2 inches at the end of Phase II testing (11.2 flight hours). An EPR (80-06-2) was submitted and is shown in appendix F. Further investigation of conditions creating burned areas (hot spots) on the IR suppressor is warranted.





CONCLUSIONS

GENERAL

- 29. The handling qualities of the UH-1H helicopter were essentially unchanged by the installation of the IR suppressor and jammer (paras 9 and 19).
- 30. Tailboom surface temperatures were generally higher than those previously reported by BHT for the initial design of the IR suppressor installation (para 22).
- 31. One deficiency has been identified as a result of the IR suppressor and IR jammer installation on the UH-III helicopter (para 27).

DEFICIENCY

32. The metal to metal contact between the engine exhaust ejector and the IR suppressor innercore support struts due to the positioning of the IR suppressor unit (para 27).

SHORTCOMINGS

- 33. The following shortcomings were identified during this test and arc listed in the order of importance:
 - a. The susceptibility of the IR suppressor unit to cracking (para 24)
 - b. The inability to latch the engine cowling in the open position (para 25)
- c. The lack of a maintenance-inspection door on the right side of the suppressor fairing (para 26).

SPECIFICATION COMPLIANCE

34. No new specification non-compliances were identified for the UH-1H as a result of the IR suppressor and jammer installation.

RECOMMENDATIONS

- 35. The following recommendations are made:
- a. Correct the deficiency listed in paragraph 32 prior to further operation with IR suppressor installed (para 27)
 - b. Correct the shortcomings listed in paragraph 33 in follow-on redesign
- c. Investigate the structual implications of the high (maximum of 340° F observed) tailboom temperatures observed during this test in follow-on redesign (para 22)
- d. Investigate the effects of the burned areas (hot spots) on the effectiveness and serviceability of the IR suppressor unit (para 28).

APPENDIX A. REFERENCES

- 1. Letter, AVRADCOM, DRDAV-DI, 21 November 1980, subject: Preliminary Airworthiness Evaluation (PAE) of the UH-1H with Hot Metal Plus Plume (HMPP) Infrared (IR) Suppressor and IR Jammer.
- 2. Test Plan, USAAEFA Project No. 80-06, Preliminary Airworthiness Evaluation of UH-1H with Hot Metal Plus Plume Infrared Suppressor and Infrared Jammer, Revision No. 1, December 1980.
- 3. Letter, AVRADCOM, DRDAV-DI, 2 February 1981, subject: Airworthiness Release for USAAEFA to Conduct a Preliminary Airworthiness Evaluation (PAE) of the JUH-1H Helicopter, S/N 69-15532 Equipped with a Garrett Hot Metal Plus Plume (HMPP) Suppressor and a AN/ALQ-144 Infrared (IR) Jammer, Project No. 80-06.
- 4. Operator's Manual, TM 55-1520-210-10, US Army Models UH-1D/H and EH-1H Helicopters, 18 May 1979, Change 10, 17 February 1981.
- 5. Detail Specification, Bell Helicopter Textron, No. 205-947-177, UH-1H Utility Helicopter FY-74 Procurement, 15 May 1973.
- 6. Military Specification, MIL-H-8501A, Helicopter Flying and Ground Handling Qualities: General Requirements for, 7 Sep 1961 with Amendment 1, 3 April 1962.
- 7. Final Report, USAASTA Project No. 66-04, Engineering Flight Test, YUH-1H Helicopter, Phase D (limited), November 1970.
- 8. Final Report, USAASTA Project No. 71-18, Tail Rotor Performance and Translational Flight Handling Qualities Tests, UH-1H Helicopter, January 1972.
- 9. Report. Bell Helicopter Textron. No 205-099-584, Results of a Test of a Model UH-1H Helicopter Equipped with an AiResearch Infrared Suppressor, 18 February 1981.
- 10. Flight Test Manual, Naval Air Test Center, FTM No. 101, Helicopter Stability and Control, 10 June 1968.

APPENDIX B. DESCRIPTION

GENERAL

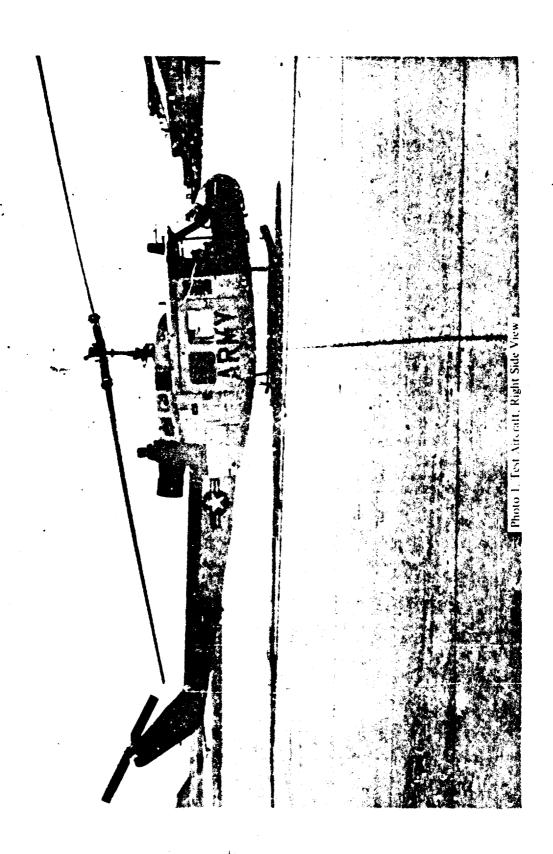
1. The test helicopter, US Army S/N 69-15532, was a production UH-1H modified to accommodate test instrumentation and the IR suppressor and IR jammer installation. The principal structural modification was the redesign of the aft engine cowling to provide support for the HMPP IR suppressor and the AN/ALQ-144 IR jammer. Photos 1 through 4 show the test aircraft with the IR suppressor, IR jammer and test instrumentation installed.

IR SUPPRESSOR SYSTEM

- 2. The IR suppressor installation consisted of four major components: the engine exhaust ejector (photo 5), the IR suppressor unit (photo 6), and an AN/ALQ-144 jammer (photo 7) which was mounted on top of the cowling assembly (photo 8). The IR suppressor is a plug-type suppressor manufactured by the Garrett AiResearch Manufacturing Company. The suppressor uses the size and shape of the plug to hide the hot engine parts. The suppressor also had circumferentially oriented vents to act as an ejector to entrain compartment and ambient air to mix with the engine exhaust, thereby reducing exhaust gas temperature. Airflow through the engine was extended aft and upward by the exhaust ejector and the IR suppressor. An insulation blanket was installed on the engine exhaust ejector.
- 3. The weight of the complete installation was approximately 127 pounds. The weight of the original aircraft components replaced by the suppressor/jammer installation was approximately 26 pounds for a net weight increase of 101 pounds. The aircraft basic weight and longitudinal center of gravity location (with test instrumentation and IR suppressor and jammer installed) was 5930 pounds at FS 142.0.
- 4. The IR suppressor and IR jammer installation evaluated during this program was a redesign of a previous installation which was reported to have caused a significant degredation in directional stability (ref 9, app A). The redesigned installation allowed both the IR suppressor and the IR jammer to be lowered in order to reduce the airflow disturbance over the vertical stabilizer.

FLIGHT ENVELOPE

5. The JUH-III with the IR suppressor and IR jammer installed was cleared for flight within the flight envelope specified in the operator's manual (ref 6, app A).

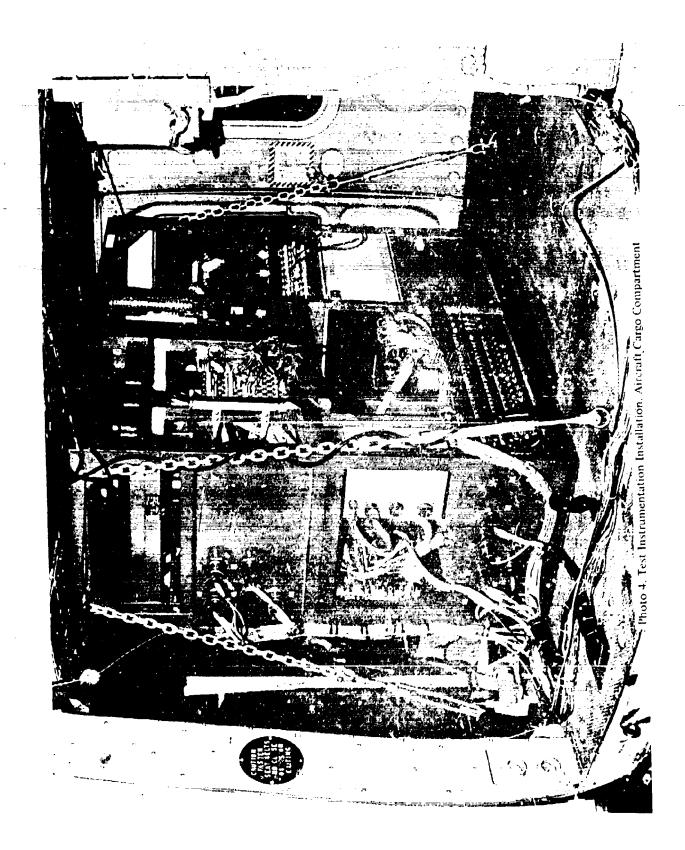


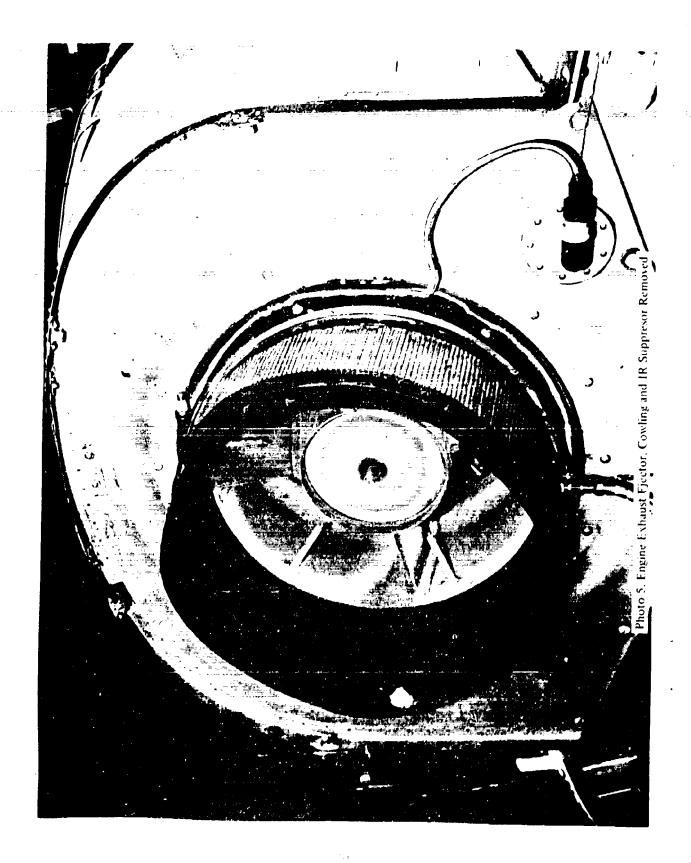
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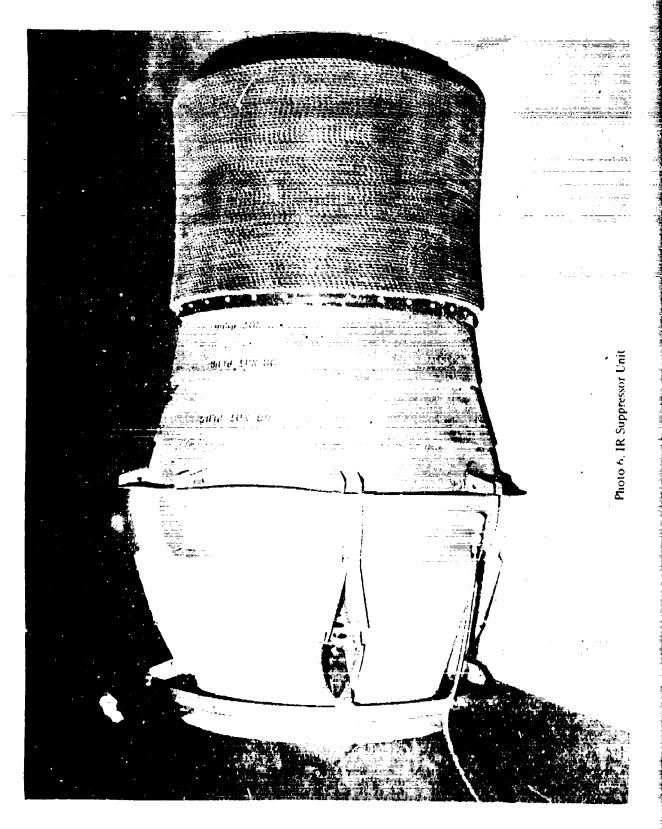


Photo 2, IR Suppressor Installation. Regin Rear. Quartering View

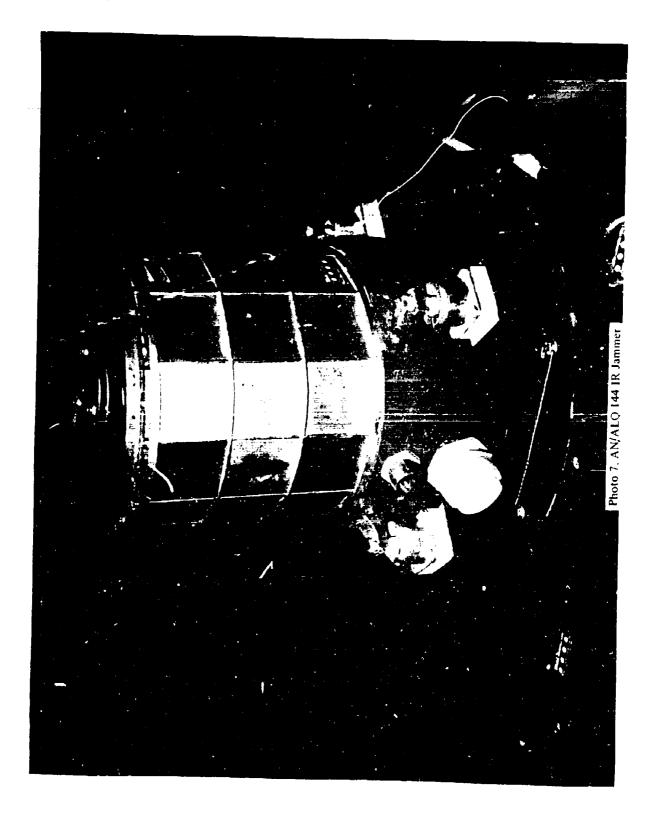
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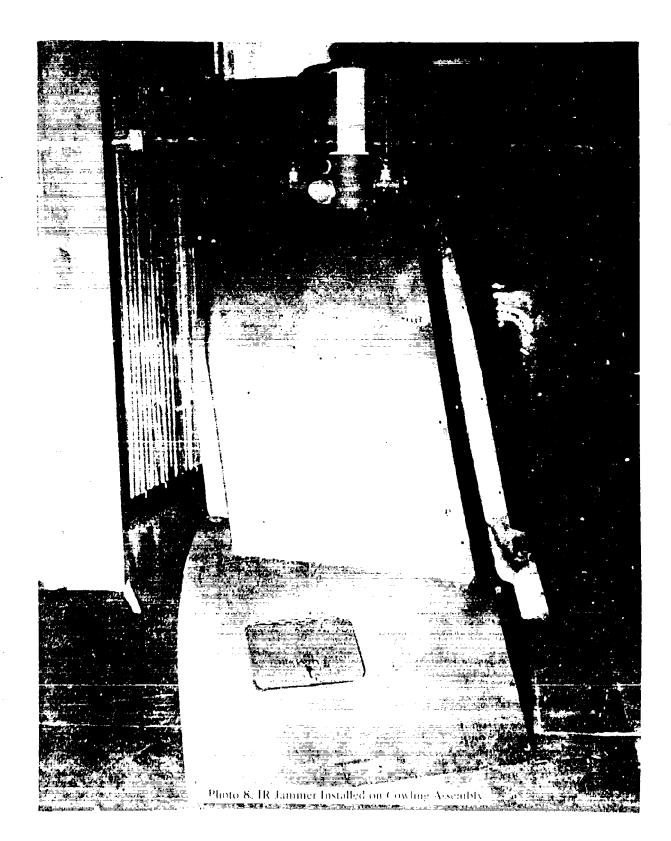






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APPENDIX C. INSTRUMENTATION

The airborne data aquisition system was installed, calibrated and maintained by USAAEFA. The system used pulse code modulation (PCM) encoding for standard handling qualities data and pressure data. Magnetic tape was used to record parameters on board the aircraft. A test instrumentation boom was mounted at the base of the aircraft windshield and extended forward for 9.5 feet. A swiveling pitot static tube and angle of attack and sideslip vanes were mounted on the boom. Temperature data were recorded by hand from a manually selectable digital display. A total of 24 thermocouples supplemented by temperature sensitive tapes were used. Pressure data were obtained using an electro/mechanical scanivalve which sequentially sampled the differential pressure. The dwell time at each sampling port was 0.5 second. Instrumentation and related special equipment installed in the aircraft and used for this test are:

Pilot Station

Event switch

Copilot Station

Instrumentation controls and displays Event switch Control fixture (jig)

Displayed on Instrument Panel

Aimpeed (boom and ship's system)
Altitude (boom and ship's system)
Angle of sideslip
Free air temperature
Control position
 Longitudinal
 Lateral
 Directional
 Collective
Rotor speed
Engine torque
Fuel used
Tape correlation counter

Hand Recorded

Temperatures (shown in table 2) Oil cooler inlet air temperature

Recorded on Tape

A. Speed (boom system)
Alutude (boom system)
Angle of sideslip
Angle of Attack
Free air temperature
Control positions
Longitudinal

Lateral Directional Collective Rotor speed Engine torque Fuel used Tape correlation counter Pitch attitude Pitch rate Roll attitude Roll rate Aircraft heading Yaw rate Throttle position Pilot's event Copilot's event Center of gravity normal acceleration Longitudinal Lateral Time Pressures (shown in table 1)

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Table 1. Pressure Sensor Locations

Pressure Port No.	Type of Measurement	Pressure Port Location
1	Static pressure	3 o'clock - 2 inches standoff at mouth of suppressor (FS 213.3)
2	Static pressure	6 o'clock - 2 inches standoff at mouth of suppressor perpendicular to center- line through (FS 213.2)
3	Static pressure	9 o'clock - 2 inches standoff at mouth of suppressor (FS 213.2)
4	Static pressure	12 o'clock + 2 inches standoff at mouth of suppressor perpendicular to center-line through FS 213.2
5	Static pressure	3 o'clock - 1 inch standoff from suppressor at FS 223.7
6	Static pressure	6 o'clock - 1 inch standoff from suppressor perpendicular to center- line through FS 223.7
7	Static pressure	9 o'clock + 1 inch standoff from suppressor at FS 223.7
8	Static pressure	12 o'clock - 1 inch standoff from suppressor perpendicular to centerline through FS 223.7
9	Total pressure	3 o'clock - surface of suppressor at first inlet
10	Total pressure	6 o'clock - surface of suppressor at first inlet
11	Total pressure	9 o'clock - surface of suppressor at first inlet
12	Total pressure	12 o'clock - surface of suppressor at first inlet
13	Total pressure	3 o'clock - surface of suppressor at second inlet
14	Total pressure	6 o'clock - surface of suppressor at second inlet
15	Total pressure	9 o'clock - surface of suppressor at second inlet

16	Total pressure	12 o'clock - surface of suppressor at second inlet
17	Total pressure	3 o'clock - surface of suppressor at third inlet
18	Total pressure	6 o'clock - surface of suppressor at third inlet
19	Total pressure	9 o'clock - surface of suppressor at third inlet
20	Total pressure	12 o'clock - surface of suppressor at third inlet
21	Static pressure	Aircraft static (boom system)

NOTE: Suppressor pressure sensor locations are illustrated in figure 1.

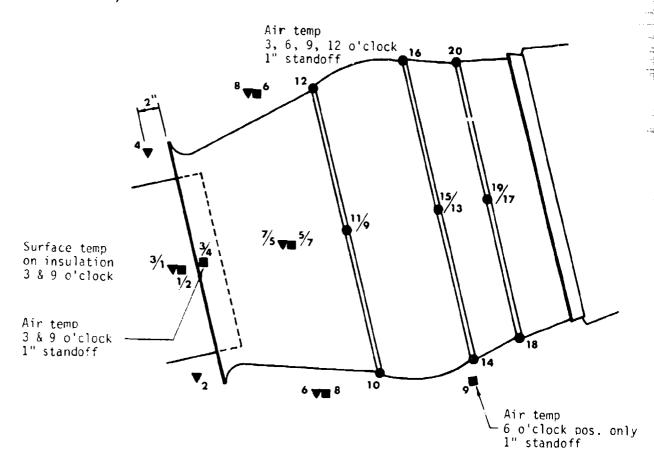
Table 2. Thermocouple and Temperature Tape Locations

Thermocouple 1 Number	Type of Measurement	Thermocouple Location
1	Surface temperature	9 o'clock - engine exhaust duct (FS 213.3)
2	Surface temperature	3 o'clock - engine exhaust duct (FS 213.3)
3	Air temperature	9 o'clock - between mouth of suppressor and engine exhaust duct (FS 215.3)
4	Air temperature	3 o'clock - between mouth of suppressor and engine duct (FS 215.3)
5	Air temperature	9 o'clock - 1 inch from suppressor surface at FS 223.7
6	Air temperature	12 o'clock - 1 inch from suppressor surface perpendicular to centerline of suppressor through FS 223.7
7	Air temperature	3 o'clock - 1 inch from suppressor surface at FS 223.7
8	Air temperature	6 o'clock - 1 inch from suppressor perpendicular to centerline of suppressor through FS 223.7
9	Air temperature	6 o'clock - between mouth of suppressor and engine centerline of suppressor through FS 236.2
10	Air temperature	Inlet to the oil cooler blower
11 - 24	Surface temperature	As illustrated in figure 2
Temperature Tape Number		

24 · 45 Surface temperature As illustrated in figure 2

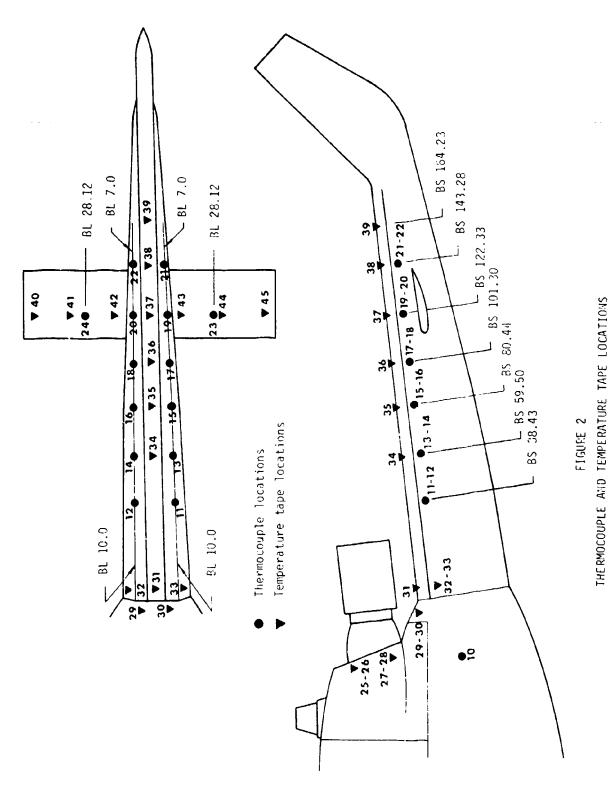
NOTE: Suppressor thermocouple locations illustrated in figure 1.

- Total Pressure 3, 6, 9, & 12 o'clock
- ▼ Static Pressure 3, 6, 9, & 12 o'clock
- Temperature thermocouples 9 o'clock/3 o'clock



■ 10 Inlet to oil cooler blower

Figure 1
Pressure and Temperature sensor locations



APPENDIX D. TEST TECHNIQUES AND DATA ANALYSIS METHODS

HANDLING QUALITIES

- 1. Stability and control data were collected and evaluated using standard test methods as described in reference 10, appendix A.
- 2. The Handling Qualities Rating Scale (HQRS) presented in figure 1 was used to augment pilot comments relative to pilot workload.

PRESSURE/TEMPERATURE SURVEY

- 3. Pressures were recorded during stabilized flight conditions using PCM instrumentation. IR suppressor pressures were referenced to aircraft boom static pressure by means of a differential pressure transducer and scanivalve. A total of 20 pressure ports on the scanivalve were used to sample the differential pressure. Pressures were measured in pounds per square inch differential (psid) and values determined by averaging the pressures recorded for each port using data plots similar to the one shown in figure 2. The location of each pressure sensor is shown in table 1, appendix C.
- 4. Temperatures were hand recorded from a selectable digital display. A total of 24 thermocouples were used. Temperature sensitive tapes were used to supplement thermocouple readings. The locations of the therocouples and temperature sensitive tapes are shown in table 2, appendix C.

AIRSPEED CALIBRATION

5. Calibrated airspeed was obtained by correcting indicated airspeed using instrument and position error corrections. The airspeed from the boom system was used for all data reduction. The calibration for the boom airspeed system used during this test is shown in figure 3.

DEFINITIONS

- 6. Definitions of deficiencies and shortcomings used during this test are shown below.
- a. Deficiency A defect or malfunction discovered during the life cycle of an item of equipment that constitutes a safety hazard to personnel; will result in serious damage to the equipment if operation is continued; or indicates improper design or other cause of failure of an item or part, which seriously impairs the equipment's operational capability.
- b. Shortcoming An imperfection or malfunction occurring during the life cycle of equipment which must be reported and which should be corrected to increase efficiency and to render the equipment completely serviceable. It will not cause an immediate breakdown, jeopardize safe operation, or materially reduce the useability of the material or end product.

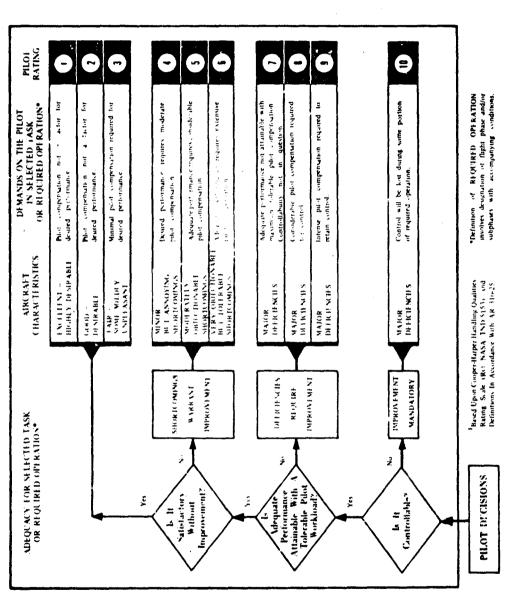
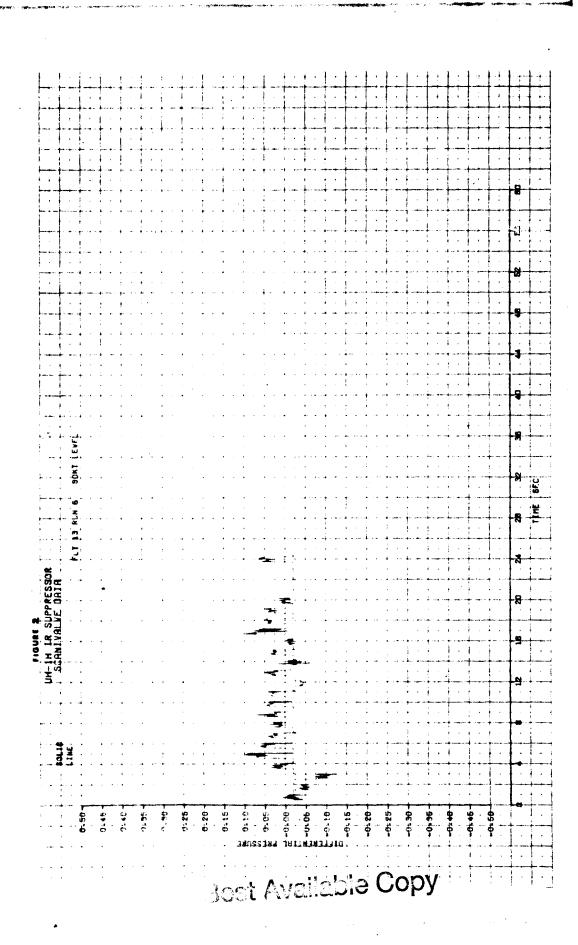


Figure 1. Handling Qualities Rating Scale



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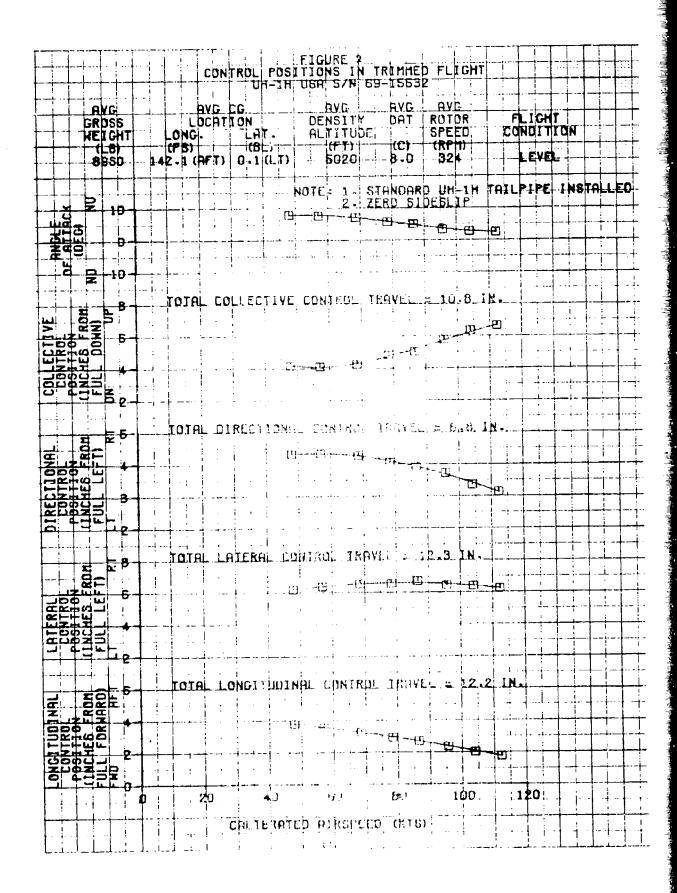
APPENDIX E. TEST DATA

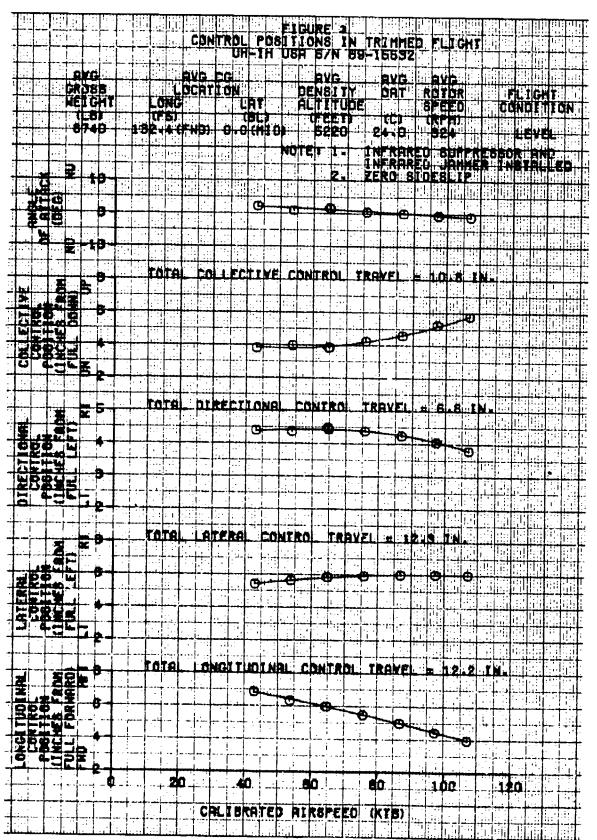
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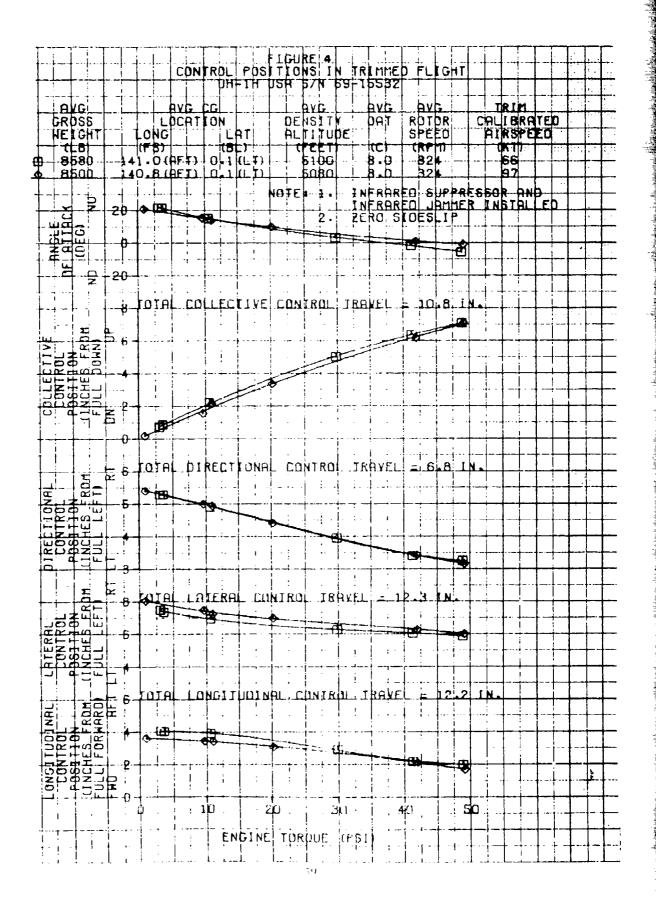
Figure	Figure Number
Control positions in trimmed flight	l through 6
Collective fixed static longitudinal stability	7 through 10
Static lateral-directional stability	11 through 14
Manuevering stability	15 and 16
Dynamic stability	
Longitudinal long period	17
Longitudinal short period	18 and 19
Lateral-directional oscillation	20 through 28
Low Speed Flight	29 through 32
Simulated engine failure	33 through 36
Pressure survey	Table 1 and 2
Temperature survey	Table 3 and 4

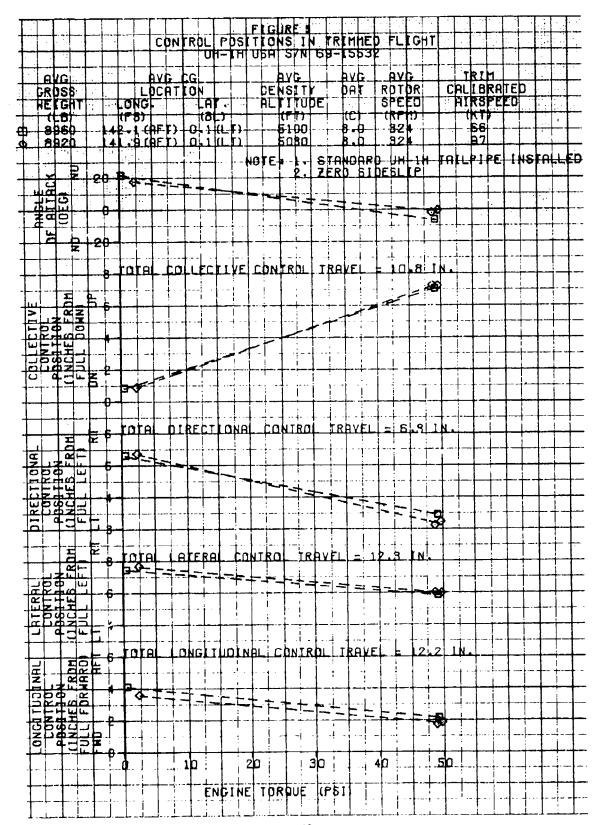
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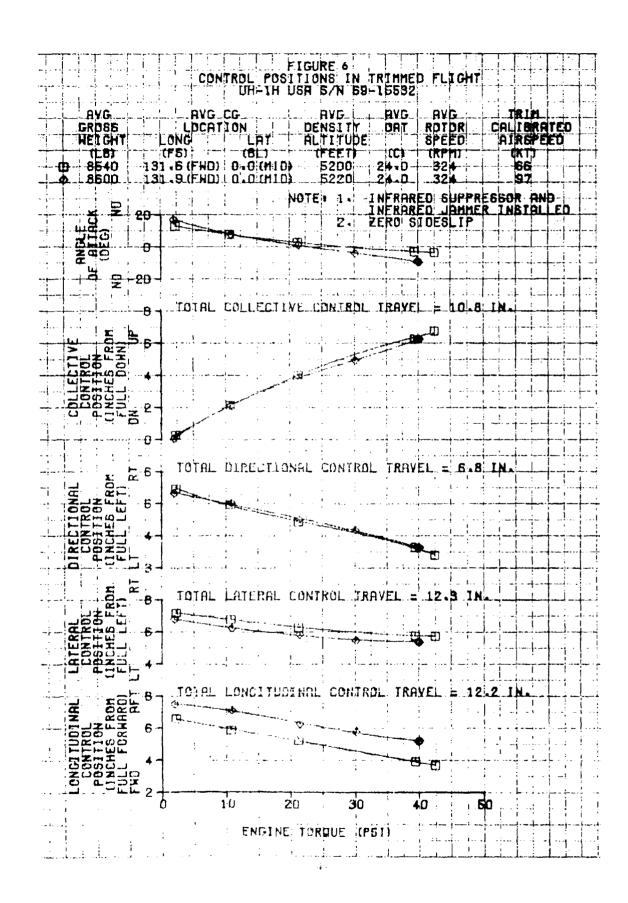
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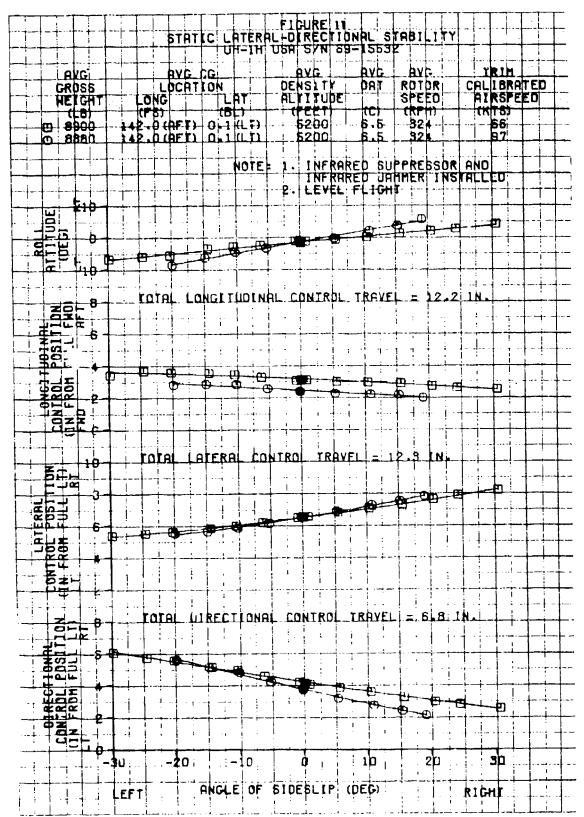


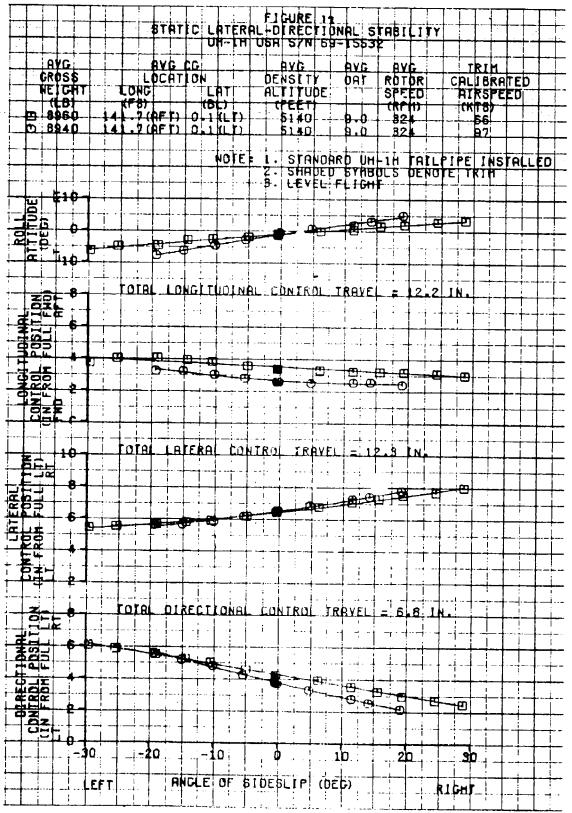
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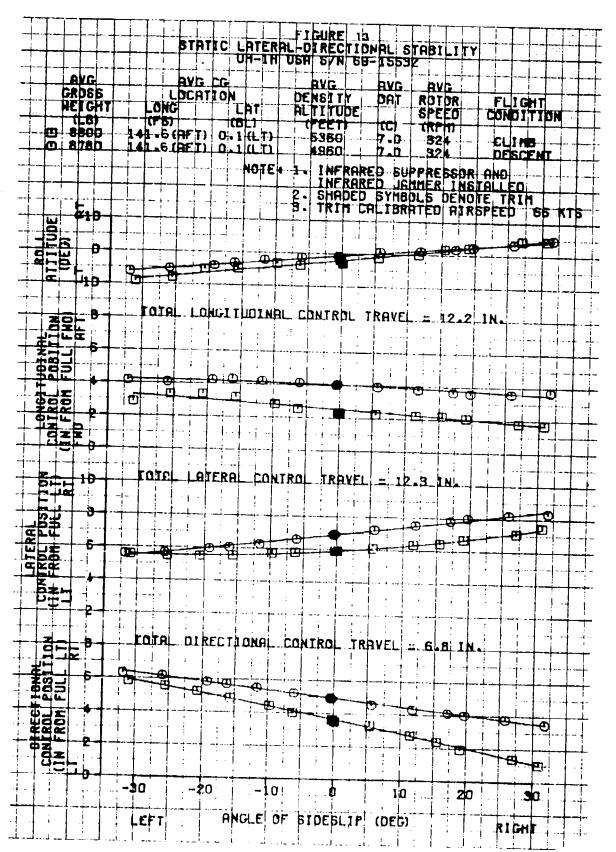
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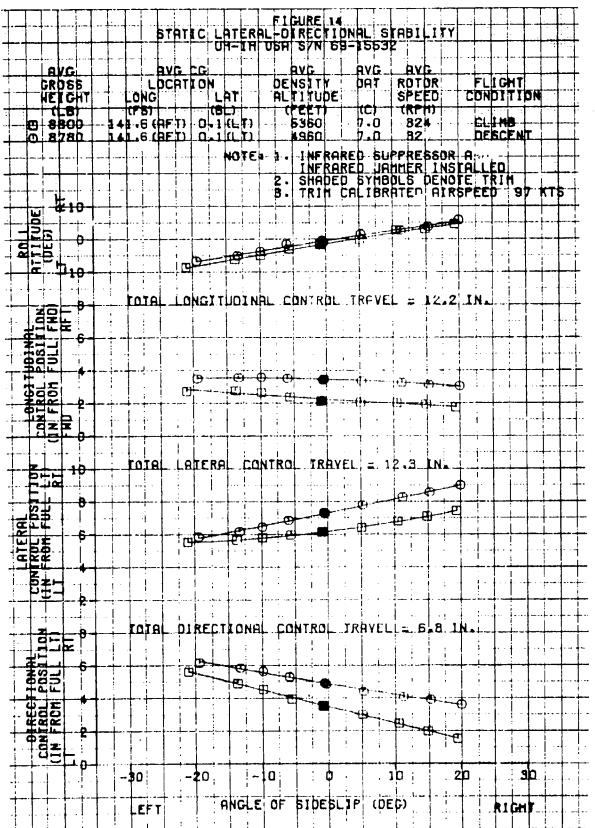
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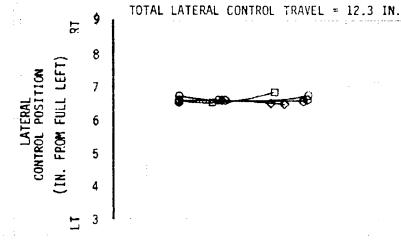


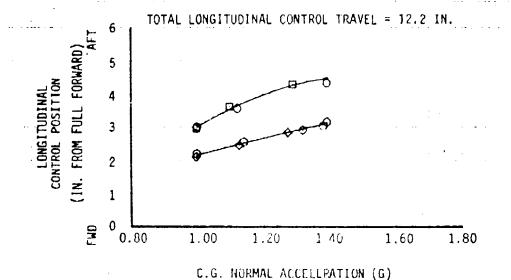


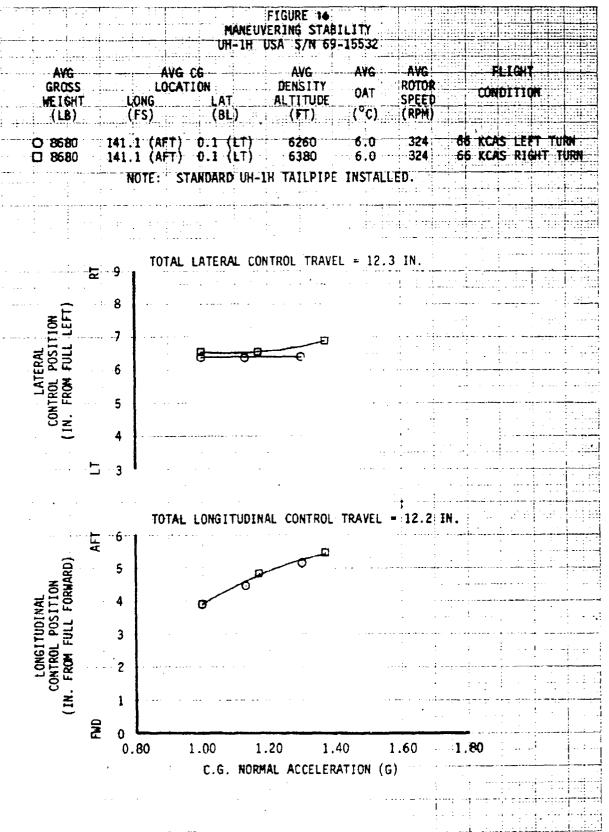
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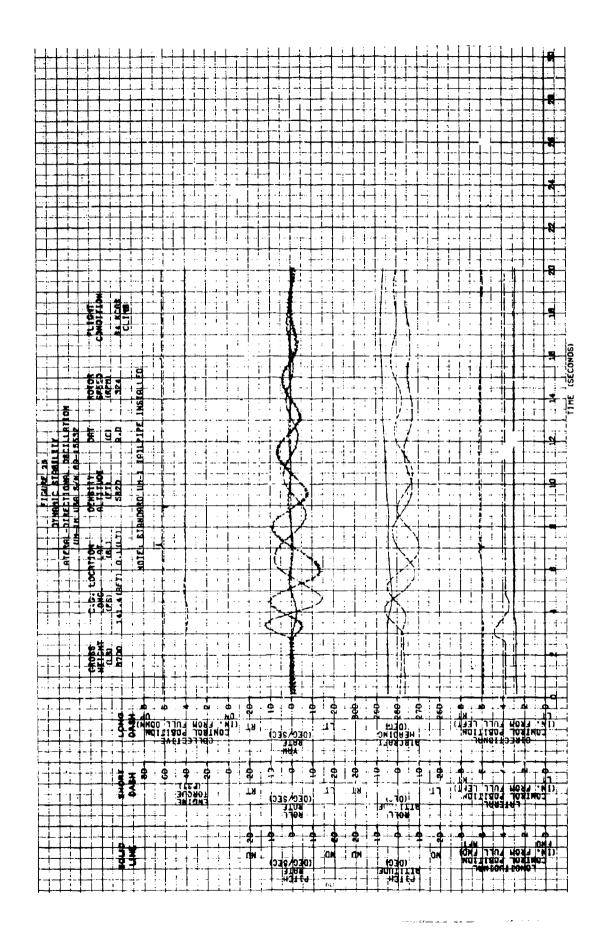
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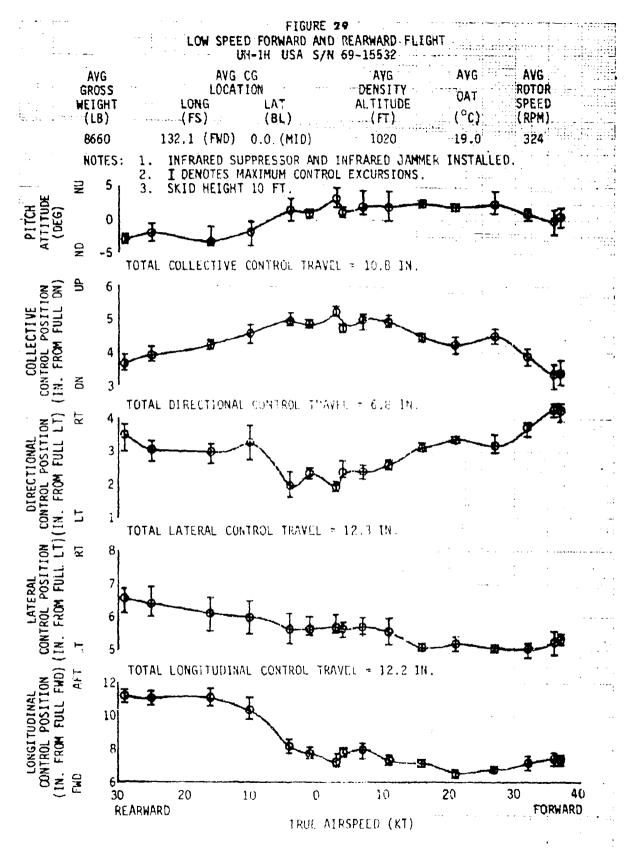


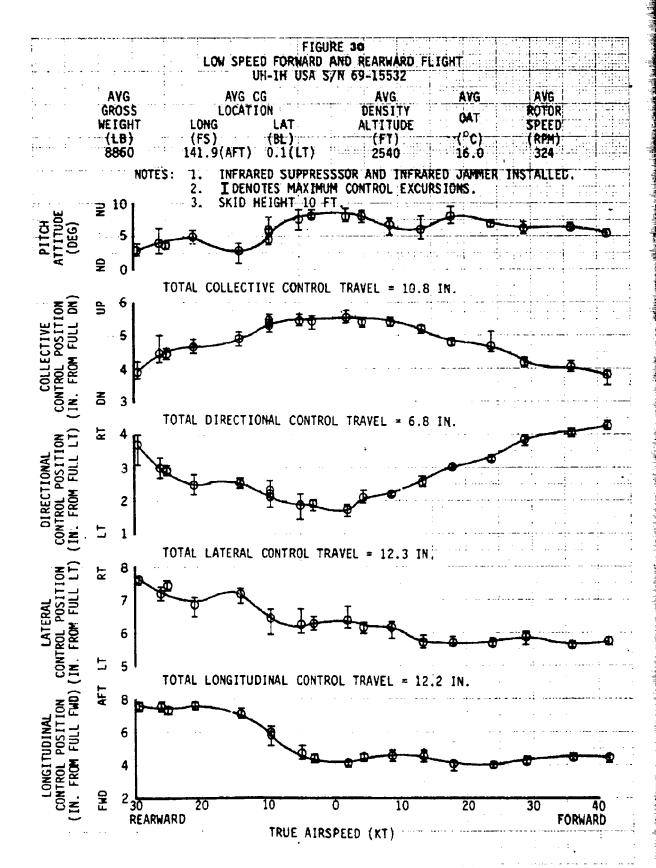
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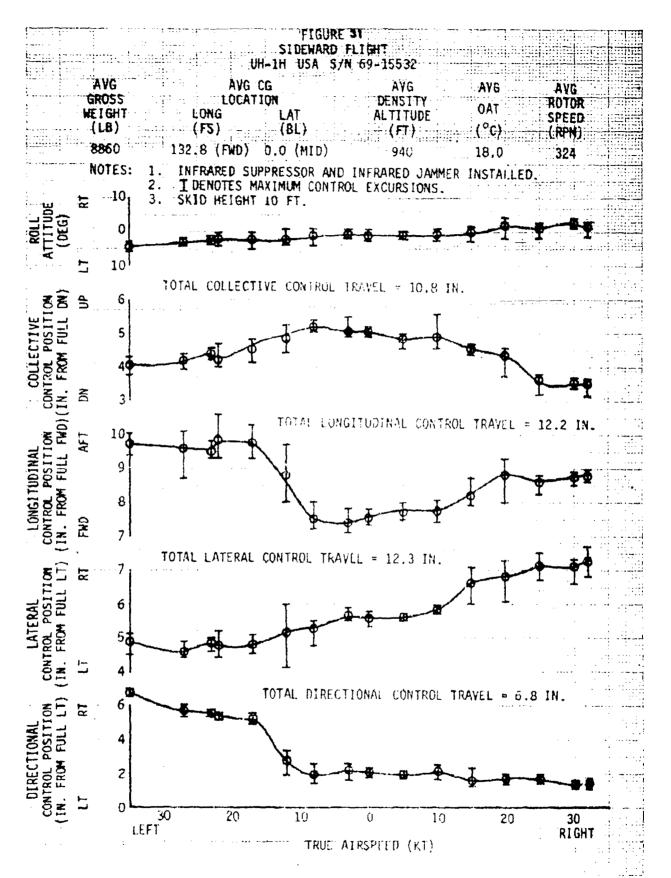
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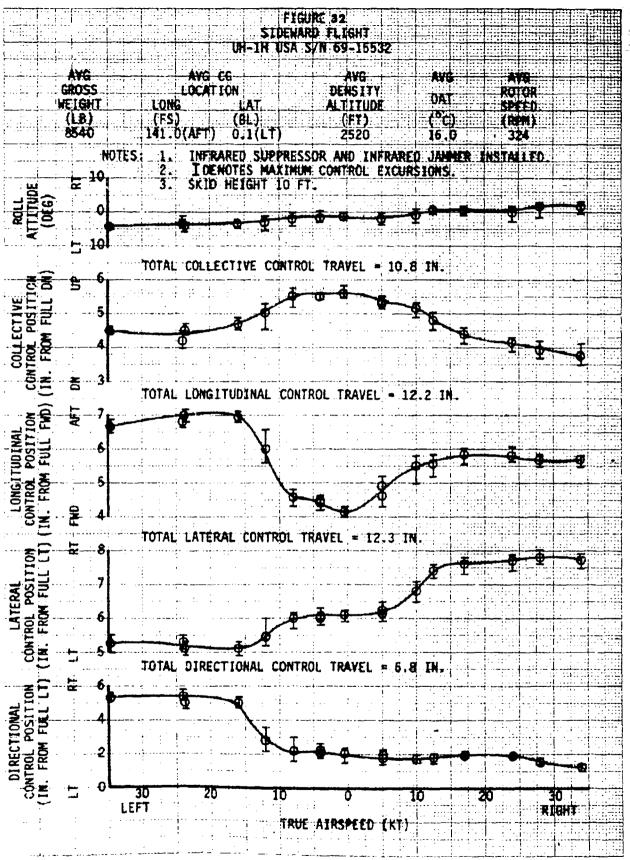
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Table 1. IR Suppressor Pressure Survey

Sensor	Document	Climb ²		Level				Side 90 K	Sideslips 90 KIAS			Autorotation
Number	mondingsor	70 KIAS	60 KIAS	80 KIAS	100 KTAS	10° L.T	20° L/F	27° LT	10° RT	20° RT	27° RT	70 KIAS
- (1 × 4	Static ³ Pressure	095 130 150	010 055 075 .005	003 030 057 .037	.017 .028 .023 .037	018 053 058 .007	017 078 022 013	048 103 .043	.005 060 .005 .070	.100 .007 0 .110	.080 .015 .028 .109	.110 .105 .110
v, € r · ∞	Static Pressure	.005 .015 .025 .035	.060 .030 .037 .037	.077 .062 .082 .032	.097 .082 .072 .047	.032 .051 .017 .052	.048 .093 .108 .093	.022 .072 .107 .037	.150 .130 .083	.240 .173 .135	.230 .180 .135	.130 .125 .125
⇒2 <u>=</u> 2	Total Pressure	050. 010. 20.0. 20.0.	.032 .042 .035 .018	.057 .057 .052 .015	.092 .084 .080	.039 .067 .103	.063 .098 .093 .088	.022 .047 .125	.090 .120 .100 .105	285 .195 .115 .165	.285 .200 .095 .167	.105 .130 .130
E ± 52	Fotal Pressure	020 -065 -010 -010	.03 .003 .03 .03 .03	280. 0 200. 700.	.077 .037 .082 .017	.027 .057 .022 .033	.008 .078 .078 .027	.008 .067 .063 .178	.070 .080 .070	.050 .140 .070 .045	.060 .150 .065 .075	.130 .130 .120 .100
7.1 81 92 92 92	Total Pressure	.010 .035 .035	037 042 027 023	.077 2.00. 2.00. 7.00.	.114 .102 .082 .035	.032 .027 .028 .028	.008	.023 028 193	.035 .075 .090 020	.160 .070 .065 .020	.165 .100 .070 .050	.115 .120 .120 .120
	Pressure Altitude	3900	4300	4300	4100	5100	4800	4400	5200	2000	4700	4200

NOTES

¹Sensor numbers correspond to location shown in appendix C.
²Indicated engine torque 40 psi.
³Pressure measured in psi differential referred to boom indicated static pressure.

Table 2. IR Suppressor Pressure Survey

	OGE		0 4	101	\prod	L 20	, v	<u>ق</u>	00	, 6	2	_ 0	စ္ဆ	<u>ي</u> د د	55.	۳	0							
Hover		8	<u> </u>	.130	3		50	_ _	010	. o		/10:-	+	080-	ŏ	Ö.	650							
I		IGE	.118	.113	0.0.	.005 010-	0	.005	.018	900.	010		.015	.020	20.	.023	550							
	۶	KTAS	.062	.090 .090	90.	-018	.00. 400.	.005	-017	600	720.	020	0.20	020	0.00	.010	200							
ward	1	K.TAS	890:-	092 102	5.	.018 610.	.007	. 032	600-	88	.025	027	50.	20.5		.017	200							
Rearward	1	KTAS		095	.045	025	010	,00	010	.003	017	-020	.035	075	040	910	200							
		KTAS	21	126	.064	.019	015 027	î	800	.002 -016	110	275-	0	.057	210.	.038	500							
		30 KTAS	-055	070	035	015	010-	900	015	015 0	035	-015	035	.030	050	025	000							
Dicht Sidoward	DINCH!	20 KTAS	-	1150	045	-015	020		010	020	035	.020	.010.	025	010.	500	903							
10:0	-	10 KTAS		899	035	015	030		010.	010	350	025	030	020	.020	-,00. -,025	30,5	Disc						
<u> </u>	- S		9	120	.040	015	010		010.	00.	1	010.	.015 210.	0.15	.020	035		200						
	Left Sideward	20 KTAS	+-	060	.025	010.	0.00	02.0.	010.	200		020	010	0	050	.040		200						
	Lef	10 KTAS		060	030	2003	20	S70-	2005	200.			. 110	0 0	001	030		200						
		40 KTAS		070	105 020	015	000	5005	0.00	0.00	010	.005	010.	25 2	010.	010.	COO.	200						
	ard,	30 7 7	CV I	- 045	- 118 - 018		000		\$00.			.005	010 905	500	0.0	010	210.	800						
	Forwa	Forw	Forw	For	Forw	Forw	Forv	202	CV IV	.045 .095	0.1. 0.0	0	<u></u> -	005	010	S00.	500:	200.	010	999	0.00	.007		200
			CV I V	103	.033				510	900 800 800	10.	0005	200	¥nn:	0.00	5003	600.	200						
	Description			State	Pressure		Static Pressure			Total Pressure			Total Pressure		, Tot	Pressure		Pressure Altitude						
		Sensor ¹ Number	-		1 ~.	eg v	. 0 ^	· x	6	2:	2	=	4 %	<u>5</u>		<u>× 2</u>	92							

NOTES

¹Sen.or numbers correspond to location shown in appendix C.
²Pressure measured in psi differential referred to boom indicated static pressure.

IR SUPPRESSOR AND TAILBOOM FEMPERATURE SURVEY

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SIMESLIPS 90 KIAS	Dale	22.72	17.7	2, 2;	<u>-</u> ;			75 : F/F:	źi.	÷;;;	(إنجر 	7. E 1 E I	ŗ.;	ান্ত্র
	78 B.L	a≢n:	177	7,7:	21.2	, ,	7.5	7, 7	7.	s, t	2	7 , %	9:	(2 건
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aldi	1990m 2011 2000m 2011	<u> </u>	• v s	· · ·		=		* /		2.2	-	£, ₹,	14.1	, X

NOTES:

1 Temperatures in degrees Celsius.
2 Thermocouple and temperature tape numbers correspond to locations shown in Appendix C. Intermocouple and temperature tape numbers correspond to locations shown in Appendix C. Minds & to lo KTS, Azimuth reletive to nose of aircraft.
4 Winds & to lo KTS, Azimuth reletive to nose of aircraft.
5 Temperature sensitive tapes were graduated in 10°E increments.
Temperatures presented are the highest indicated by the tape, converted to degrees Celsius.

Best Available Copy

IR SUPPRESSOR AND TAILBOOM TEMPERATURE SURVEY TABLE 41

:arward,		49 43 43 44 49 49 49 111 111 110 110 110 110 110 110 110 11	
٤, ۲ ₁₉	Temperatur Tape Mumb	25 27 27 28 28 33 34 34 34 34 34 45 45 46 47 48 48 48 48 48 48 48 48 48 48 48 48 48	
	30 KTAS	8 E E S C C C C C C C C C C C C C C C C C	23
RIGHT	20 KTAS	88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	33
ex.	10 KTA®	25	23
	30 KTAS	8 8 9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	 C1
LEFT	20 KTAS	25	
	10 KTAS	8 2 2 2 2 3 3 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	77
	30 KTAS	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	92
REARWARD	20 KTAS	4	25
33	10 KTAS	8 2 2 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	54
	40 KTAS	# 7-10-2 # # 11 # 12 # 12 # 2 # 2 # 2 # 2 # 2 #	2
5	30 KTAS	85 98 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	20
FORWARD	20 KTAS	- 0 2 1 2 8 1 2 8 1 2 9 2 1 2 8 1 2	20
	SATM 01	# \$1111 # C + 60 C - 0 \$12 # # # # # # # # # # # # # # # # # # #	2
<u>د</u>	491	847811114198848886 <u>1</u> 5688888	7,
HOVER	-l'20	883739945 <u>64773</u>	23
əjd	TocomorT TodonN	- 0m+ 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	AMB

NOTES

¹ Temperatures in degrees Celsius.

² Thermocouple and temperature tape numbers correspond to locations shown in Appendix C.

³ Temperature sensitive tapes were graduated in 10°F increments.

Temperatures presented are the highest indicated by the tape, converted to degrees Coisius.

75

APPENDIX F. EQUIPMENT PERFORMANCE REPORTS

Commander		Cornander						
U.S. Army Aviati	Ion RùD		on	Engineering Fligh				
4300 Goodfellow		Activity ATTN: DAVTE-TA (STop 217)						
St. Louis, MO	63120	TaEdwards. (AFS, C)						
i i	TECOM/AVSCOM PROJ NO.:	Prelim Eval of U						
80-06-1	USAAEFA 80-03	Suppressor and D						
4. MODEL		TEM PATA						
	<u> 10H-1H </u>	5. SERIAL NO. 69-15!	32					
B MFR:	one	9. USA 40.:						
o mr x:	11.04							
10. NOMENCLATURE/DESCRIPTION	5	RT DATA						
11, FSN:	Exhaust Duct	12, MFR PART NO.: Bell p/n	205	060 017 1				
13, DRAWING NO.:								
IS QUANTITY:		16. NEXT ASSEMBLY:	ÇOP	ter Textrom				
17. MAC FUNCTIONAL GRP:		18. PART TEST LIFE:		 -				
	III INCID	ENT DATA						
19. DATE OF OCCURRENCE:	THE THE TAX TO SEE TH	20. TYPE OF REPORT:	21.	ACTION TAKEN:				
22. MAINT SPT, ELM, CODE:		a INCIDENT	1	a REPLACED				
23. OBSERVED DURING	24. TEST ENVIRONMENT.	b. INFORMATION _	+	b. REPAIRED				
X a. OPERATION	Suspect that damage	25. INCIDENT CLASSIFICATION:	1	c. ADJUSTED				
b. MAINTENANCE	occurred during	O CRITICAL	†	d. DISCONNECTED				
INSPECTION	sideward or rearward	y & MAJOR	X	. REMOVED				
4. OTHER	flight	c. MINOR	+	1. NONE				
*	IV INCIDENT	DESCRIPTION						
		N MAC CODE IDENTIFIED IN BLOCK 22): -4), it was noted that there was damage to						
the exhaust duct (191 suppressor bellmouth. the leading edge of t struts indicate that Looking at the exhaus position, approximate the suppressor strut I suspect two possible	134-1-1) where the exhall the exhaust duct is the IR suppressor strut there has been "\footnote " lat duct from the rear only \footnote inch of duct metal contacted the duct. e causes: (1) The exhall	ust duct fits internall warped out of shape and sinside the bellmouth, eral flexing or movement the aircraft at the land has been pushed forwards. (2) The IR suppress	y i l ha . S it a . to .rd	nto the IR s been contacting core marks on the gainst the strut 2 o'clock and torn where be against the				
too close to the exhaparticular it appears may move the suppress Recommend that the suppress outer ring of the exhaparte prevent warpage.	that the new gusset su that the new gusset su or further forward aga appressor be reposition aust duct be reinforce	f the new fairing and b pport (Bell p/n 205-038	ulk 3-21 oca	head rework. In $6-121$ and -122)				
27. DEFECTIVE MATERIAL SENT		Y						
28. NAME, TITLE & TEL EXT C	!'REMARER	29. FOR THE COMMANDER:						
DRAM ENVIORTH								
CA-4 AV350-4785								
M1333-4100		ì						

EQUIPMENT PERFORMANCE REPORT (DARCON ANCR 7(M)-38)

8 June 1981

DAVTE-TA

OFFICE SYMBOL:

EQUIP	MENT PERFORMANCE REPO	RT	DATE. 30 HUL 81
Commander	DARROW MICE TOWN		DAYTE -TA
US Army Aviation ATTN: DRDAV-D 4300 Goodvellow St. Louis, MO	RAD Command 31vd. 03120	ATTV: E Edwards	er my Aviation Engr Flt Activity DAVTE-TA, Stop 217 AFB, CA 93523
1 (PR NO	The Wagner William	· TEST HISE	
80-05 -2	80-05	UH-1H I	IR Suppressor
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	H PA	RT DATA	
किक साथ इस्ते छ। । जा	To a Garrett Hype IR Su	opi essor.	
Fi. I. S.		Se	erial Mo. 129-417
E. CANAMA . No.		14 W Garrett	AiResearch
The Award of the congress of t	417	ใ้ ระบบได้ ค.ป. การีสุดสลาย !!!!!!	
कर, संक्रा राज्य है। किया है।		* * * * * * * * * * * * * * * * * * *	
	III INCID	ENT DATA	
A CONTROL OF MARKS	13 ACR-18 MAY 21	Tak a Kelai Eta	21. ACTION TAKEN:
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F. Markett Markett	Francis Comps		d DISCONNECTED
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e company of the second second second second second	IV INCIDENT	DESCRIPTION	
program was obse- by discoloration surface aft of a	ryen in caye developed to cat to 3. 13. 2. and 4 c no negative enints. Thes top one, Eurober invest	our burned areas ofclock positions ser hat spots" ap	pheared as shown in the
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US Army Research and Technology Laboratories/Aeromed	chanics
Laboratory (DAVDL-ATL-D)	1
US Army Research and Technology Laboratories/Propulsion	on
Laboratory (DAVDL-PL-D)	1
Defense Technical Information Center (DDR)	12
US Military Academy (MADN-F)	
MTMC-TEA (MTT-TRC/Steve Hola)	1